

# The effect of Am241 on UK plutonium recycle options in thorium-plutonium fuelled LWRs

## – Part I: PWRs

S. L. Morrison<sup>1</sup>, and G. T. Parks<sup>2</sup>

<sup>1</sup>*University of Cambridge: Engineering Department, Trumpington Street, Cambridge, CB2 1PZ.  
slm85@cam.ac.uk*

<sup>2</sup>*University of Cambridge: Engineering Department, Trumpington Street, Cambridge, CB2 1PZ.  
gtp10@cam.ac.uk*

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### Abstract

UK plutonium is expected to be managed using uranium-plutonium (U-Pu) mixed oxide (MOX) fuels in Light Water Reactors (LWRs). However, studies have shown that thorium-plutonium (Th-Pu) may be preferential. Research has mostly focussed on recycle of reactor grade Pu with limited minor actinide (MA) content. This study will determine if large quantities of americium (Am) in UK Pu may be restrictive to recycle schemes by determining the effect this has on reactivity feedback coefficients, fissile loading and incineration potential. Addition of Am is shown to result in predictable trends in reactivity feedback coefficients and spatial separation of Am and Pu is found to offer potential advantages over uniformly loaded fuel in terms of maximising fissile loading and incineration. Separation may also offer benefits in terms of targeting Am destruction, particularly if multiple recycle schemes are pursued, as this would maximise the fissile loading requirements while keeping reactivity feedback coefficients negative.

## 1. Introduction

### 1.1. UK Pu stockpile

The UK has accumulated a substantial stockpile of civil Pu from decades of operating nuclear power plants and reprocessing the spent fuel. The isotopic quality of the stockpile varies significantly due to the different reactor types that have been operated historically in the UK, their various fresh fuel compositions and typical discharge burnups, and the storage times associated with different ‘batches’ of reprocessed fuel. One option for managing the stockpile is long-term disposal in a waste repository. However, there are not-insurmountable engineering challenges associated with designing a long-term storage facility. With this in mind, the UK government may wish to give further consideration to alternatives such as transuranic recycling in current or advanced reactor technologies.

In its current state, UK Pu is estimated to contain roughly 4%wt Am241, which has accumulated from the decay of Pu241 (Gill, 2016). Given that the UK is due to cease all reprocessing activities by 2020 (Department for Business, Energy & Industrial Strategy, 2018) (Nuclear Decommissioning Authority, 2018), it is reasonable to assume that any recycle scheme adopted may include burning of Am241 in-

situ. There are, therefore, two key points to consider when assessing the viability of UK Pu recycle, namely the in-core performance of:

1. Pu-only-bearing fuels from recently reprocessed spent fuel, and
2. Pu-Am241-bearing fuels from aged spent fuel.

### **1.2. Viable technologies for Pu disposition**

Many studies have considered transuranic (TRU) waste incineration using existing technologies (Galahom, 2018) (Mohamed & Badawi, 2016) (Sahin, et al., 2012a) (Sahin, et al., 2012b), while others have considered advanced options, including but not limited to: Fast Reactors (FRs) (Wallenius & Bortot, 2018) (You & Hong, 2016) (Wider, et al., 2014) (Tucek, et al., 2008) (Bays, 2007); Molten Salt Reactors (Waris, et al., 2015) (Heuer, et al., 2014); Small Modular Reactors (Zou, et al., 2018); Pebble Bed High Temperature Reactors (Acir & Coskun, 2015); High Temperature Gas-cooled Reactors (Lennox, et al., 2007); and Accelerator Driven Systems (Al Qaaod, et al., 2018). However, it has been determined that, for the purposes of UK Pu incineration, MOX fuelled Light Water Reactors (LWRs) may provide the ideal platform for Pu disposition (Nuclear Decommissioning Authority, 2014) (Institution of Mechanical Engineers, 2013) (Department of Energy & Climate Change, 2011) (International Atomic Energy Agency, 2003) (The Royal Society, 1998). Some studies have suggested a two-fold management scheme utilising both fast and thermal systems (Collins & Renier, 2006) (Zaetta, 2004). However, deployment of a FR fleet would likely be a longer-term option. Since the UK is moving towards expanding its LWR fleet, it is expected that thermal reactors may form the basis for recycle in the short- to medium-term (Office for Nuclear Regulation, 2017) (Nuclear Industry Association, 2015) (Office for Nuclear Regulation, 2012).

While standard U-Pu MOX options have been considered (Gul, et al., 2018) (Salam & Hah, 2018) (Alonso, et al., 2018) (Ramirez, et al., 2016) (Haas & Hamilton, 2007) (Cowell & Fisher, 1999) (Schlosser, et al., 1993), studies have shown that Th-Pu MOX may provide a promising alternative (Ernault, et al., 2015) (Lau, et al., 2014) (Revol, et al., 2013) (National Nuclear Laboratory, 2012) (Fridman & Kliem, 2011) (International Atomic Energy Agency, 2005) (International Atomic Energy Agency, 2002) (Galperin, 1995) (Cadelli & Lippens, 1988) (Shapiro, et al., 1977). The high conversion ratio and lack of breeding of additional Pu in the Th-cycle results in significantly lower Pu / MA content in discharged fuel compared to standard U-Pu MOX, leading to potentially lower levels of radiotoxicity and decay heat of associated waste materials compared to standard UO<sub>2</sub> and U-Pu fuels (Hesketh & Thomas, 2013) (International Atomic Energy Agency, 2005). In addition, potential improvements in Th-fuel based safety margins may be achievable: in particular, the potential for more favourable reactivity feedback coefficients and the possibility of increased proliferation resistance of spent fuel (Raitses, et al., 2012) (Yun, et al., 2010) (Shwageraus, et al., 2004) (Weaver & Herring, 2003) (Lombardi, et al., 1999) (Galperin & Raizes, 1997). While there are notable downsides to the Th-fuel cycle, specifically the lack of commercial infrastructure and the reduced worth of certain control materials (du Toit & Naicker, 2018) (Alhaj, et al., 2016) (Lau, et al., 2014) (Insulander Bjork, et al., 2013) (Fridman & Kliem, 2011) (Lamarsh & Baratta, 2001), it may warrant further investigation. Th-Pu only recycle has been studied in depth (Zainuddin, et al., 2017) (Alhaj, et al., 2016) (Zainuddin, et al., 2016) (Tucker, et al., 2015) (Yun, et al., 2010) (Mittag & Kleim, 2011) (Schram & Klaassen, 2007) (Sorensen, et al., 2006) (Kim & Downar, 2002) (Galperin, et al., 2000). However, it is Th-Pu-MA recycle that is of more interest with respect to UK Pu management due to the previously mentioned build-up of Am241. While some studies have addressed Am-specific recycle, these have typically focussed on U-fuels (Houas, et al.,

2016) (Hyland & Gihm, 2011) (Grouiller, et al., 2003) (Delpech, et al., 1998). (Bays, et al., 2009) summarised findings of U-Am transmutation studies, concluding that transmutation of Am<sup>241</sup> in a thermal spectrum reactor loaded with MOX fuel may be a viable recycle option (Cesana, et al., 2004). Part I of this study will consider Pu-Am recycle in Pressurized Water Reactors (PWRs) while Part II will consider Boiling Water Reactors (BWRs).

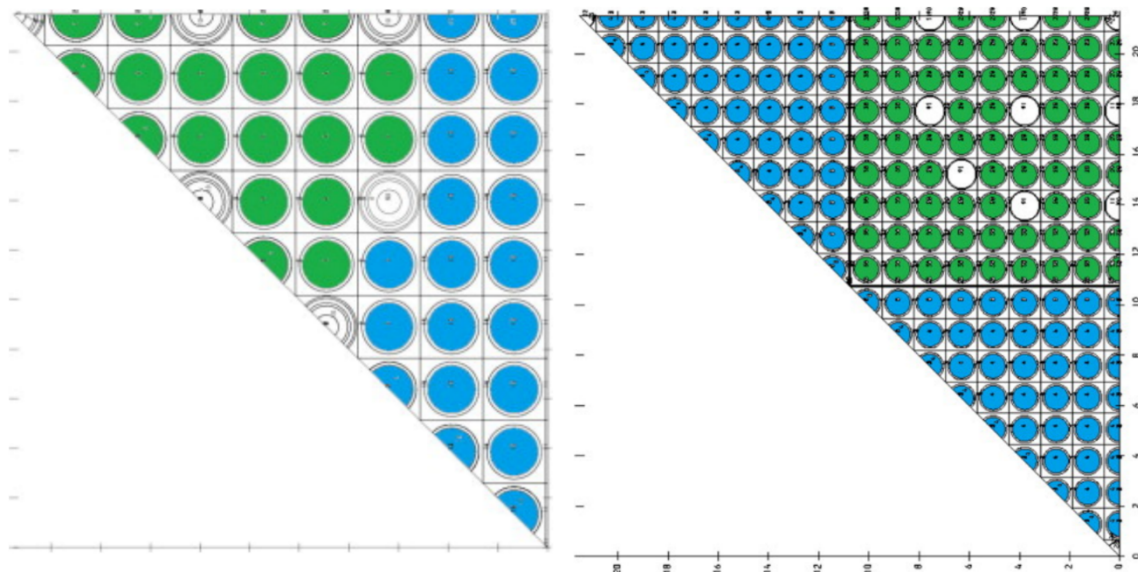
The incineration capability of Pu/MAs in PWRs is strongly dependent on neutron energy and this, in turn, is determined by the degree of moderation that occurs within the reactor. Moderation can be altered in several ways and the effects can be exploited in order to target incineration in different isotopes or for the purposes of fulfilling different fuel performance objectives. One way to alter the degree of moderation and the overall neutron energy spectrum is to vary the hydrogen-to-heavy-metal (H/HM) ratio. Previous research has shown that there are benefits associated with increased, standard and reduced moderation in PWRs for single and multiple stage recycle schemes as summarised by (Morrison, et al., 2018). Given that there has, as yet, been no decision regarding whether a single or multiple stage scheme will be pursued, both PWRs and reduced moderation PWRs (RMPWRs) will be considered. In addition to the effect of moderation, it may also be advisable to consider spatial separation of 'clean' and 'dirty' Pu from the UK stockpile in order to best target destruction of Am, which, if not efficiently incinerated, may give rise to unacceptably high fresh fuel and/or reload requirements, resulting in positive temperature coefficients of reactivity. Spatial separation has previously been demonstrated to be neutronically advantageous due to the ability to target TRU incineration and improve neutron economy by placing Th-TRU in faster spectrum locations while placing, in most cases, fissile U bred from Th (U<sup>233</sup>) in softer spectrum locations (Rahman, et al., 2012). Spatial separation can be achieved in a number of ways: for example, heterogeneous loading of fuel within a single assembly where Th-TRU pins may be placed at the centre of the assembly and Th-U<sup>233</sup> pins at the periphery (TCUP), or through whole assembly heterogeneity (WATU) (Figure 1). Studies comparing TCUP to WATU showed that both designs allowed a satisfactory discharge burnup to be achieved while maintaining a negative Moderator Temperature Coefficient (MTC); however, reactivity was found to become positive for a beyond design basis loss of coolant accident (LOCA) (Lindley, et al., 2014a) (Lindley, et al., 2014b). Adequate shutdown margins were achievable in both cases, though this required the use of B<sup>10</sup>-enriched B<sub>4</sub>C rods. Limiting the pin power peaking was found to be difficult for the WATU design, resulting in a high axial form factor and an unacceptable total hot channel factor. The study concluded that the TCUP layout was, on balance, the preferable design, and it will therefore be considered in this study for the purpose of achieving spatial separation of Am within UK Pu.

When considering spatial separation of Am and Pu, it may be wise to place an upper limit on the heavy metal content of the fuel. Limiting the total Pu content of the fuel may be beneficial to avoid reaching the saturation point for energy produced from U<sup>233</sup> (Kotlyar, et al., 2017a) while Am content will be limited to a theoretical maximum based on current and projected manufacturing capabilities. This is due to the presence of strong alpha and gamma emitters and the difficulties that these introduce with regards to safe handling of Am<sup>241</sup>-bearing fuels. The Nuclear Decommissioning Authority have suggested that the Am content of UK Pu should ideally not exceed ~4% if it is to be recycled before 'additional treatment costs' start being incurred. However, they note that the UK Pu stockpile will likely exceed this limit in some instances, with THORP derived Pu expected to contain up to 10% Am after several decades' storage (Nuclear Decommissioning Authority, 2010) (Nuclear Decommissioning

Authority, 2009). Am-bearing fuels have been successfully manufactured with up to 10%wt Am (French Alternative Energies and Atomic Energy Commission (CEA), 2015) and, if there is appropriate justification, a maximum of 30% may theoretically be achievable<sup>1</sup>. (Collins, et al., 2007) determined that, due to the negative breeding effects of Pu241, it may be ideal to allow decay to Am241. Cooling periods of 30+ years, resulting in ~75% reduction in Pu241 inventories, were suggested. In the case of the UK stockpile, this cooling period has been achieved for some of the older batches of spent nuclear fuel.

Since the UK stockpile will contain varying amounts of Am depending on the decay time of individual batches, and Am content may be higher if it is further separated from Pu to allow fabrication of concentrated Am pins, this study will consider Am limits up to and including the predicted maximum amount of Am that can be feasibly included in manufacture.

**Figure 1 TCUP (left) and WATU (right) designs for spatial separation of TRU (blue) and U3 (green) (Lindley, et al., 2014b)**



### 1.3. Effect of Am on performance

Before undertaking a detailed analysis of the benefits of separating Pu/Am, it may be useful to determine how sensitive key in-core safety parameters are to increases in Am loading. Previous research has shown that the presence of Am in UK Pu, and its addition to Th-Pu MOX fuel, results in a flatter effective multiplication factor ( $k_{eff}$ ) versus burnup curve compared with standard grades, due to the absorption peaks of Am241 existing at higher energies than the main fission peaks of fissile isotopes (Morrison, et al., 2018). This results in a greater fraction of neutrons being absorbed during

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<sup>1</sup>Pu238 ( $T_{1/2} = 88$  years) has historically been limited to ~6% in MOX fuel (Baetsle, 1995). Am241 has a significantly lower heat burden but similar alpha-decay energy properties to Pu238. Therefore, it may be assumed that the maximum %wt Am that can be included in manufacture can be determined from the maximum %wt Pu238. Since the half-life of Am241 is five times greater ( $T_{1/2} = 432$  years) than Pu238, the maximum %wt can reasonably be scaled by a factor of 5, resulting in a maximum theoretical %wt of ~30% for Am241.

moderation. Increasing the Am content of the fuel with a view to flattening the keff curve may offer potential advantages in terms of a smaller reactivity swing, which may potentially reduce the burden on reactivity controls. This would be advantageous given that Th-fuels are already associated with increased control requirements. However, it was shown that MTC and Void Coefficient (VC) are highly sensitive to changes in the neutron energy spectrum, brought about by varying the isotopic composition of the fresh fuel and/or altering the hydrogen-to-heavy-metal (H/HM) ratio and so trends observed in the previous study may not necessarily indicate how UK Pu might perform when the Am241 content is varied. Adding Am will harden the spectrum, which may be beneficial if perturbations cause the average neutron energy to shift away from the major resonant fission peaks of fissile isotopes such as Pu239 and Pu241 or towards the major resonant absorption peaks of Am241; however, it may be disadvantageous if it results in a shift in average neutron energy towards the key resonant fission peaks of U233 (at end-of-cycle (EOC)) or causes an unacceptable increase in fast fissions in both fissile and fissionable isotopes (including Am241 itself). In addition, increases in the amount of Am241 will result in higher fissile loading requirements to maintain an acceptable keff throughout the cycle. This increases the likelihood that MTC and VC will become positive. The only potential offset against the positive contributions to reactivity feedback coefficients in fuels with a higher fissile content is breeding of Am242m from Am241. Am242m has the largest fission cross section in the thermal energy region and this decreases with increasing neutron energy. Reductions in moderator/coolant density may therefore result in large negative reactivity feedback effects as the average neutron energy increases.

Once it has been determined if there are any predictable trends in the MTC/VC response of UK Pu with increasing Am content, total Pu/Am limits can be identified and the efficiency of different lattice types can be considered from the point of view of maximising total Pu loading and achieving suitable Pu/Am incineration rates. Based on these findings, the benefits of spatial separation can be considered in comparison to uniform fuel loading.

## **2. Method**

### **2.1. Pu vectors and model set-up**

Different UK Pu vectors are considered for an initial single-pass recycle study in standard and reduced moderation PWRs in order to determine the effect of varying the Am content of the fuel. These compositions have been based on the predicted UK Pu vector and have been scaled in line with increasing Am content. The first three Pu vectors detailed in Table 1 consider three bounding cases for the UK Pu stockpile based on a single lumped mass Pu vector:

1. Recently reprocessed, and therefore isotopically 'clean', Pu (0%wt Am),
2. Isotopically averaged 'as is' Pu (3.91%wt Am), and
3. Aged Pu, where all Pu241 has decayed to Am241 (5.60%wt Am).

The additional Pu vectors assume incremental increases in Am241 up to 30%wt.

**Table 1 Isotopic composition of plutonium vectors**

	Am content (%wt)	Isotopic composition (%wt)					
		Pu238	Pu239	Pu240	Pu241	Pu242	Am241
Clean	0.00	0.2498	68.7689	26.7041	1.7588	2.5185	0.0000
As is	3.91	0.2400	66.0800	25.6600	1.6900	2.4200	3.9100
Aged	5.60	0.2400	66.0800	25.6600	0.0000	2.4200	5.6000
	10.00	0.2248	61.8920	24.0337	1.5829	2.2666	10.0000
	15.00	0.2123	58.4535	22.6985	1.4950	2.1407	15.0000
	16.00	0.2098	57.7658	22.4315	1.4774	2.1155	16.0000
	17.00	0.2073	57.0782	22.1644	1.4598	2.0903	17.0000
	18.00	0.2048	56.3905	21.8974	1.4422	2.0651	18.0000
	19.00	0.2023	55.7028	21.6303	1.4246	2.0400	19.0000
	20.00	0.1998	55.0151	21.3633	1.4070	2.0148	20.0000
	23.00	0.1923	52.9520	20.5622	1.3543	1.9392	23.0000
	30.00	0.1748	48.1382	18.6929	1.2311	1.7629	30.0000

Assembly-level calculations were performed using the established reactor physics code WIMS (version WIMS10A) (Lindley, et al., 2017) (Askew, et al., 1966) and nuclear data library ENDF/B-VII (Chadwick, et al., 2006). An initial benchmarking study was carried out against published data for a Th-Pu fuelled, standard PWR (International Atomic Energy Agency, 2003) to ensure the accuracy of the model. Results were generated by first performing an approximate flux solution using 172 neutron energy groups with geometric approximations inherent to the code (Lindley, et al., 2017) and then by performing a more detailed final solution using 47 groups and the method of characteristics. Thermal and epithermal region energies are split into a larger number of groups than the fast region, as these represent the energy ranges where most interactions occur in standard and reduced moderation PWRs. Burnup calculations were performed and perturbations to temperature, density and boron concentration were included. Comparisons were made for the infinite multiplication factor ( $k_{inf}$ ) as a function of burnup and reactivity feedback coefficients (MTC, Doppler Coefficient and Boron Worth) and pin-by-pin power distributions were compared for beginning-of-cycle (BOC) and EOC. Results showed good agreement, with minor discrepancies being attributed to the differences in the older, unspecified codes and data libraries used in the IAEA study and the code used in this study. Additional validation was carried out using the Monte Carlo code Serpent (Leppanen, 2015) to determine the accuracy of results for larger perturbations (VC (fully voided)).

The benchmarked model was adapted such that a standard 17 x 17 PWR lattice, similar to those used in Sizewell B, could be compared to a RMPWR (reference geometry and operational parameters outlined in Table 2). The fuel pin diameter was increased from 9.5 mm in the PWR to 11.0 mm in the RMPWR to reduce the H/HM ratio in line with previously proven feasible designs (Lindley, 2014). Each assembly contained 264 zircaloy-clad fuel pins and 25 empty water holes.

**Table 2 Reference assembly geometry and operating conditions**

Parameter	PWR	RMPWR
Fuel pellet radius (cm)	0.4095	0.4845
Fuel pin radius (cm)	0.4750	0.5500
Lattice pitch (cm)		1.26
Fuel temperature (K)		900
Cladding temperature (K)		600
Moderator temperature (K)		585
Moderator density (g/cc)		0.7007
Boron concentration (ppm)		500
Assembly power (kW/cm)		6.19 <sup>2</sup>

The theoretical densities of PuO<sub>2</sub> and ThO<sub>2</sub> were assumed to be 11.5 g/cc and 10.0 g/cc respectively. For all fuel materials used, the assumed density is 95% of their corresponding theoretical density. For purposes of comparison, several design constraints were fixed: the soluble boron concentration was fixed at 500 ppm; the assembly linear power rating was assumed to be ~6.2 kW/cm; and thrice-burned fuel was expected reach a total discharge burnup of 60 GWd/tHM. For a three-batch fuel management scheme with a discharge burnup of 60 GWd/tHM, keff of 1.03 (or more) was required up to 40 GWd/tHM. This keff value accounts for the effects of neutron leakage, which is typically ~3% in PWRs.

## 2.2. Reactivity feedback coefficients

Changes in reactivity for MTC and VC were calculated using Equation 1.

$$\Delta\rho = \frac{k_{\infty}^p - k_{\infty}^n}{k_{\infty}^p \cdot k_{\infty}^n} \frac{1}{\Delta X}$$

**Equation 1**

where  $n$  and  $p$  refer to nominal and perturbed conditions respectively and  $X$  represents the change in moderator temperature or % voiding outlined in Table 3.

**Table 3 Perturbed operating conditions**

Coefficient	Perturbation
MTC	moderator temperature +5 K moderator density reduced to 0.6886 g/cc
VC (90% void fraction)	moderator density reduced to 0.07 g/cc <sup>3</sup>
VC (fully voided)	moderator density reduced to 0.01 g/cc <sup>4</sup>

## 2.3. Isotopic contribution to reactivity feedback coefficients

Isotopic contributions to reactivity feedback coefficients are determined as per (Ganda & Greenspan, 2010). Where “the major contributors to the reactivity coefficient are fissile isotopes, it is more

<sup>2</sup> Assumed equal to the assembly power of Sizewell B when fuelled with 3.1% enriched UO<sub>2</sub> (Meyer & Stokke, 1997)

<sup>3</sup> Representing a 90% void fraction (VF) as per typically accepted regulatory limits (AREVA/EDF, 2012)

<sup>4</sup> Representing an extreme LOCA

convenient to rank the constituent contribution by the number of fission neutrons they emit per neutron absorbed in the system". Normalizing "per absorbed neutron",  $k_{\infty}$  is broken down as per Equation 2:

$$k_{\infty} = \eta \cdot f = \frac{\sum_j \nu_j \Sigma_{fj} \Phi_j}{\sum_i \Sigma_{ai} \Phi_i} = \frac{\nu_1 \Sigma_{f1} \Phi_1}{\sum_i \Sigma_{ai} \Phi_i} + \frac{\nu_2 \Sigma_{f2} \Phi_2}{\sum_i \Sigma_{ai} \Phi_i} + \dots$$

$$= \frac{\nu_1 \Sigma_{f1} \Phi_1}{\Sigma_{a1} \Phi_1} \cdot \frac{\Sigma_{a1} \Phi_1}{\sum_i \Sigma_{ai} \Phi_i} + \frac{\nu_2 \Sigma_{f2} \Phi_2}{\Sigma_{a2} \Phi_2} \cdot \frac{\Sigma_{a2} \Phi_2}{\sum_i \Sigma_{ai} \Phi_i} + \dots$$

**Equation 2**

Defining  $\eta$  and  $f$  as:

$$\eta_j \equiv \frac{\nu_j \Sigma_{fj} \Phi_j}{\Sigma_{aj} \Phi_j} ; \tilde{f}_j \equiv \frac{\Sigma_{aj} \Phi_j}{\sum_i \Sigma_{ai} \Phi_i}$$

**Equation 3**

$k_{\infty}$  may then be described by:

$$k_{\infty} = \eta_1 \tilde{f}_1 + \eta_2 \tilde{f}_2 + \dots$$

**Equation 4**

where:

$\eta_j$  is the total number of fission neutrons produced per neutron absorbed in component  $j$   
 $\tilde{f}_j$  is the fraction of neutrons absorbed in component  $j$  from the total neutrons absorbed in all system constituents. This definition differs slightly from the standard thermal utilization definition.

Change in reactivity due to perturbations in moderator density can then be defined as per Equation 5:

$$RFC = \frac{k_{\infty}^p - k_{\infty}^n}{k_{\infty}^p \cdot k_{\infty}^n} \frac{1}{\Delta T} = \frac{1}{\Delta T} \frac{(\eta_1 \tilde{f}_1|_p - \eta_1 \tilde{f}_1|_n) + (\eta_2 \tilde{f}_2|_p - \eta_2 \tilde{f}_2|_n) + \dots}{k_{\infty}^p \cdot k_{\infty}^n}$$

**Equation 5**

### 3. Results and discussion

#### 3.1. Neutron multiplication

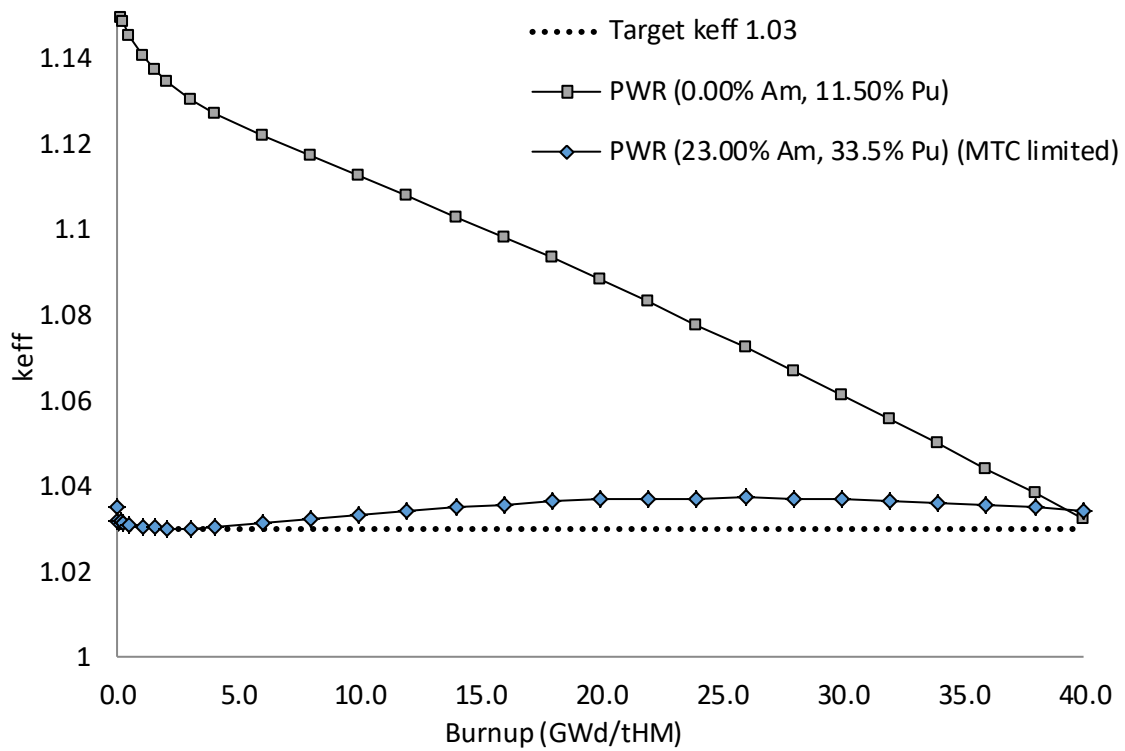
To achieve a sufficient keff, the total Pu content was varied depending on the Am content of the fresh fuel and the lattice type being considered. For low Am content cases, the keff curve decreases with increasing burnup in both the PWR and RMPWR. However, for higher Am content cases, there is a slight reduction in keff early in the burnup cycle prior to an increase in keff as the cycle progresses (Figure 2). This is due to the absorbing properties of Am241 and the daughter products that exist in the transmutation chain, as discussed by (Morrison, et al., 2018). For lower Am content cases, the RMPWR requires a higher total Pu fraction in the fresh fuel to achieve the desired keff, while, for higher Am content cases, the PWR requires a higher total Pu fraction in the fresh fuel (Figure 3). As the Am content increases the difference in the total Pu requirements for the two lattice types increases.

Where a negative MTC is required, the maximum allowable Am content in the fuel is 23%wt in the PWR (33.50%wt total Pu) and 16%wt in the RMPWR (22.50%wt total Pu). If the fuel composition is constrained by the need to maintain a negative VC (fully voided), the maximum allowable Am content

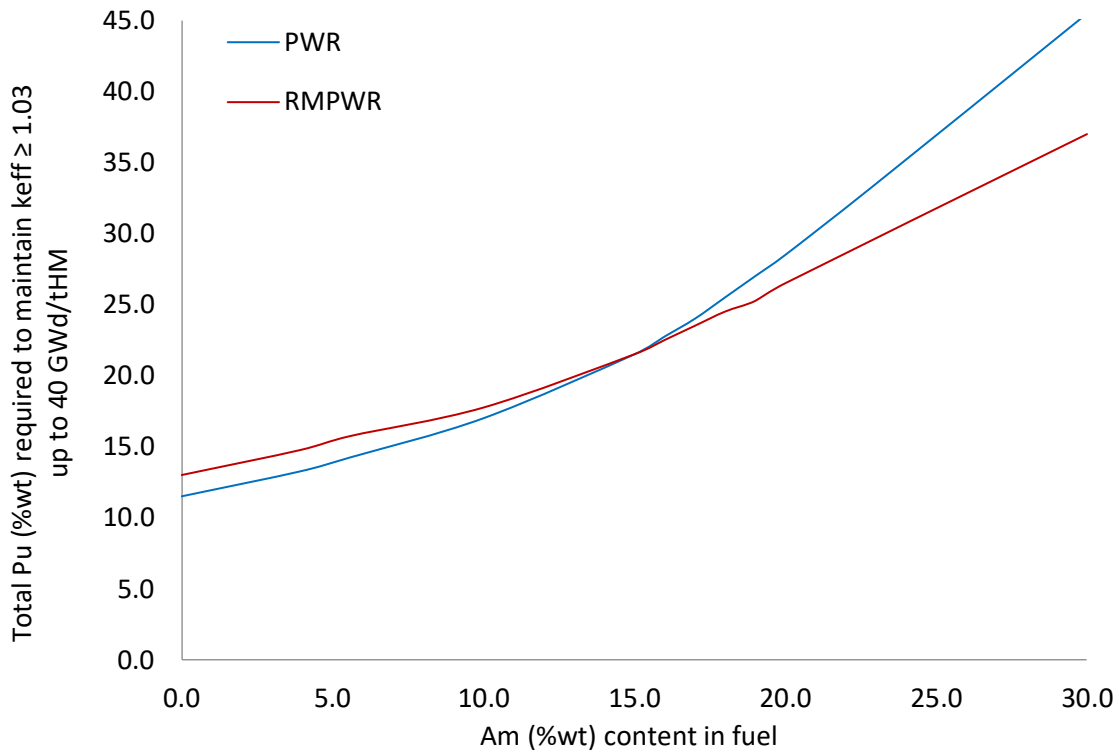


of the fuel is again higher for the PWR (10%wt Am, 17.00%wt total Pu) than the RMPWR (5.60%wt Am, 15.75%wt total Pu). For each of the scenarios considered, the effect of increasing Am was recorded and the isotopic contributions towards total MTC and VC have been determined to identify key trends and overall effect on the sign and magnitude of the coefficients.

**Figure 2 Typical keff-burnup curves for UK Pu with different Pu and Am %wt content**



**Figure 3 Total Pu required to maintain  $k_{eff} \geq 1.03$  up to 40 GWd/tHM for varying Am content**



### 3.2. MTC

Figure 4 plots the variation of MTC with burnup for selected cases. It shows that, as expected, the addition of Am causes the MTC to become less negative due to the hardening effects of the presence a thermal neutron absorber and the increased Pu loading requirements that this causes. From an isotopic point of view, a harder spectrum results in a reduction in the magnitude of negative contributions from key fissile isotopes, such as Pu239, and an increase in the magnitude of the positive contributions from fissionable isotopes, such as Am241 and Pu240 (Figure 5), which ultimately leads to a less negative MTC. Perhaps unexpectedly, the MTC is consistently more negative in the PWR than the RMPWR, despite the significantly higher fraction of total Pu required to maintain an acceptable  $k_{eff}$  in the high Am cases in the PWR.

In the lower Am content cases, the MTC is more negative overall in the PWR, because the negative contributions from Pu239 and Pu241 are typically greater in the PWR than the RMPWR, while the positive contributions from all other isotopes, including fissile U233, are greater in the RMPWR. In the higher Am content cases, the contributions from most isotopes are similar regardless of reactor type. However, the discrepancy in the contributions from Pu239 (i.e. negative in the PWR and significantly less negative/more positive in the RMPWR) is large enough that the PWR continues to display an overall more negative MTC than the RMPWR.

In particularly high Am content cases, the total magnitude of contributions from Pu239 is overshadowed by the positive effects from fissionable isotopes, particularly Am241 and Pu240. This is due to the hardening of the spectrum causing a shift away from the fission peak of Pu239 such that, despite the Pu239 fraction of the fuel outweighing Pu240 and Am241 by 20–30%wt, these fissionable isotopes begin to dominate. For very high Am content cases such as 30% Am, the negative

While the fissile fraction of the fresh fuel and the presence of fissionable isotopes dictate whether the MTC is positive or negative, it is the effect of Pu239 and, to a lesser extent, Pu241 which appears to dictate which lattice type has the more negative MTC.

Figure 10 is a line graph showing the Maximum Temperature Coefficient (MTC) in pcm/K versus Burnup in GWd/tHM for various reactor configurations. The y-axis ranges from -50.0 to 40.0 pcm/K, and the x-axis ranges from 0.0 to 40.0 GWd/tHM. Six data series are plotted:

- PWR (0.00% Am, 11.50% Pu): Blue dashed line, MTC starts at approximately -42 pcm/K and decreases slightly to -44 pcm/K.
- RMPWR (0.00% Am, 13.00% Pu): Red dashed line, MTC starts at approximately -35 pcm/K and increases slightly to -32 pcm/K.
- PWR (18.00% Am, 25.50% Pu): Blue dash-dot line, MTC starts at approximately -20 pcm/K and increases slightly to -18 pcm/K.
- RMPWR (18.00% Am, 24.5% Pu): Red dash-dot line, MTC starts at approximately 2 pcm/K and decreases slightly to 0 pcm/K.
- PWR (30.00% Am, 45.50% Pu): Blue solid line with open circles, MTC starts at approximately 19 pcm/K and decreases slightly to 17 pcm/K.
- RMPWR (30.00% Am, 37.00% Pu): Red solid line with open circles, MTC starts at approximately 31 pcm/K and decreases slightly to 27 pcm/K.

Isotope

MTC contribution (pcm/K)

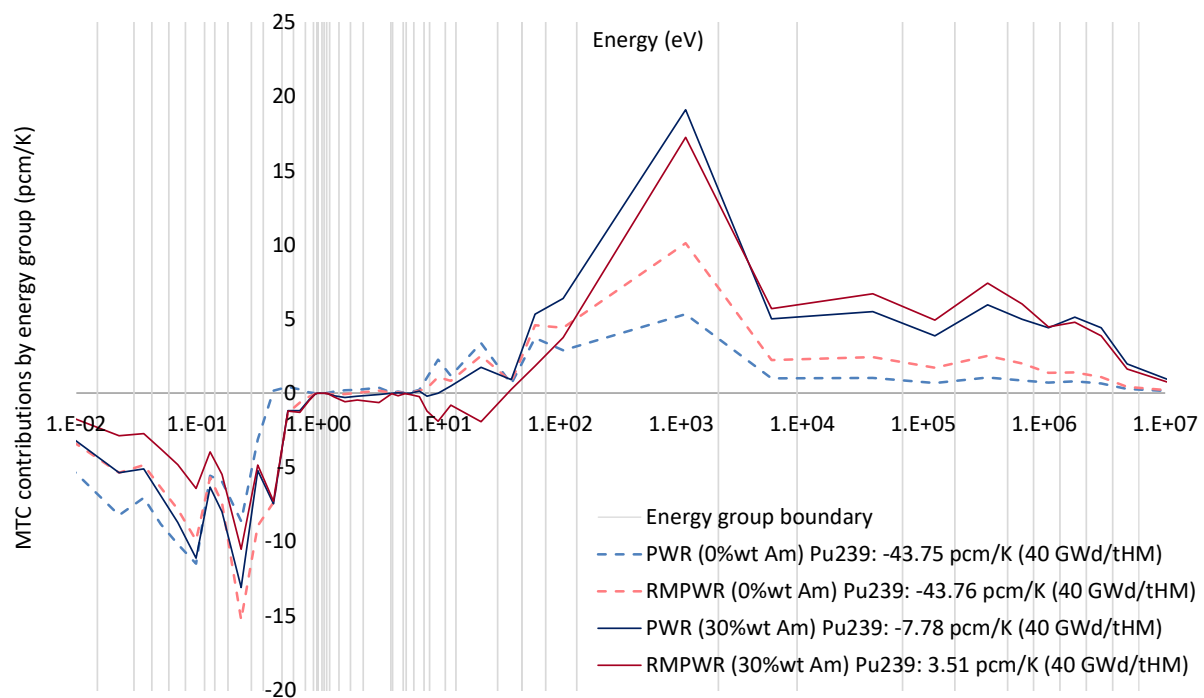
Am241 Pu238 Pu239 Pu240 Pu241 Pu242 Th232 U233 Am242 Am242m

Legend:

- PWR (0% Am) EOC
- PWR (18% Am) EOC
- PWR (30% Am) EOC
- RMPWR (0% Am) EOC
- RMPWR (18% Am) EOC
- RMPWR (30% Am) EOC

Figure 6 illustrates how the contributions from Pu239 vary with neutron energy for both lattice types considered with increasing Am/Pu content. It shows that the negative contributions in the thermal energy region are always greater in the PWR than the RMPWR regardless of Am content and total Pu loading. This is attributable to the energy distribution of neutrons and the subsequent effect that this has on the energy-averaged microscopic cross section of the isotope. There is a higher thermal flux in the PWR than the RMPWR (Figure 7), which is more noteworthy in the lower Am case due to this being a softer, more thermal spectrum than higher Am cases. Fissile isotopes such as Pu239 have an increasingly large microscopic cross section with decreasing neutron energy in the thermal energy range, hence there is greater negative reactivity feedback in the PWR, because, while the perturbation in moderator density from 0.7007 to 0.6886 g/cc results in a fairly equal change in flux in the PWR and the RMPWR, the average neutron energies for the nominal and perturbed cases are lower (and therefore sit further to the left of the energy spectrum) in the PWR than in the harder spectrum of the RMPWR. This results in a greater difference in the average cross section between nominal and perturbed cases in the PWR than the RMPWR. It is worth noting that, for thermal energies in the range 0.1–1 eV in the low Am case, the RMPWR displays a more negative thermal contribution than the PWR. This is because there is a large peak in the cross section of Pu239 at this energy and, since the RMPWR has a harder spectrum, the perturbation in this case results in a shift towards this peak and a subsequent negative reactivity feedback effect. As the spectrum hardens with increasing Am/Pu content, the average neutron energy ‘misses’ this peak and the effect is lost.

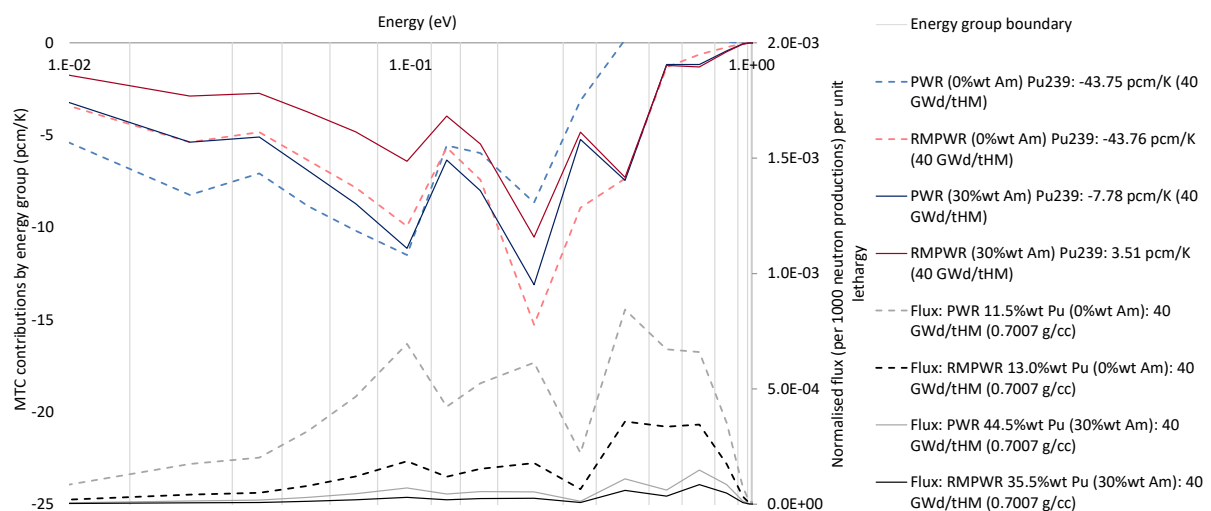
**Figure 6 Contributions to MTC from Pu239 for 0 and 30%wt Am cases in the PWR and RMPWR at 40 GWd/tHM**



In the lower Am content cases, the negative contributions from Pu239 are far more significant than the positive epithermal contributions. A combination of a greater magnitude in negative thermal contributions and a smaller magnitude in positive epithermal contributions results in a more negative total contribution towards MTC in the PWR. As the Am/Pu content increases and the spectrum hardens, the negative thermal contributions decrease and the positive epithermal contributions

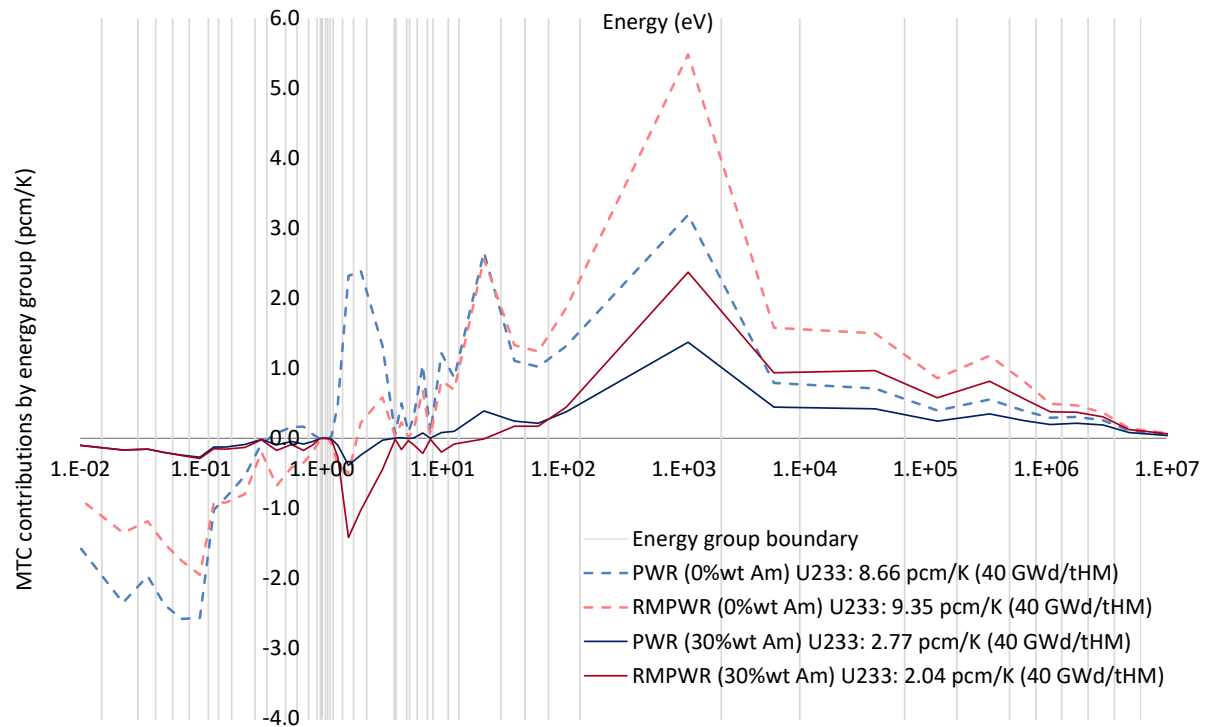
increase. The positive epithermal contributions are more comparable in the higher Am/Pu content cases despite the difference in total Pu loading. This is because the proportion of neutrons existing at this energy is similar due to the reduction in moderation in the RMPWR and the higher fissile content in the PWR. However, the reactivity feedback in the thermal energy region, though diminished, remains significantly more negative in the PWR due to the difference in cross sections. It is this feature which causes the overall MTC to remain more negative in the PWR in the higher Am content case.

**Figure 7 Thermal energy contributions to MTC (above, left-hand axis) from Pu239 for 0 and 30%wt Am cases in the PWR and RMPWR at 40 GWd/tHM compared with normalised flux (per 1000 neutrons produced) per unit lethargy (below, right-hand axis)**



The same effects are noted in the response of Pu241, since this isotope displays a similar cross section and resonance structure to Pu239. A different trend is observed in the response of U233, due to the key fission peak of this isotope existing at a slightly higher energy than those of Pu239 and Pu241. While U233 has a consistently positive effect on MTC, the magnitude of the positive contributions diminishes with increasing Am/Pu content due to increased competition with Pu239, and a change in trend is observed regarding which lattice type displays the larger positive contribution overall. In lower Am content cases, the difference in fissile loading (higher total Pu content in the RMPWR) and the effect of reduced moderation means that there is a notably harder spectrum in the RMPWR. This leads to a significantly more positive contribution in the epithermal energy region of the RMPWR than the PWR (Figure 8). This outweighs the greater negative effects in the thermal region of the PWR and the large positive reactivity effect caused by a shift in average neutron energy towards the first resonant peak of U233 in the energy range 1–10 eV. In the higher Am content cases, there remains a more significant positive contribution in the epithermal region of the RMPWR than the PWR; however, the spectrum has been hardened such that the negative thermal contributions are negligible and the perturbation in moderator density results in a shift away from the major resonant peak of U233. This shift in neutron energy results in a large negative contribution in the energy range 1–10 eV. The overall effect is that the larger positive epithermal contributions in the RMPWR are overshadowed by the negative contribution at 1–10 eV, resulting in a smaller total positive contribution in the RMPWR than the PWR.

**Figure 8 Contributions to MTC from U233 for 0 and 30%wt Am cases in the PWR and RMPWR at 40 GWd/tHM**



There is also a change in trend for Am241. This isotope displays a more positive contribution in the RMPWR in cases with low Am content in the fresh fuel, while a more positive contribution is observed in the PWR in cases with higher Am content. This is due to greater fast fission effects in the harder spectrum of the RMPWR in lower Am content cases and greater fast fission effects in the PWR in higher Am content cases caused by the higher total Pu content in the fuel.

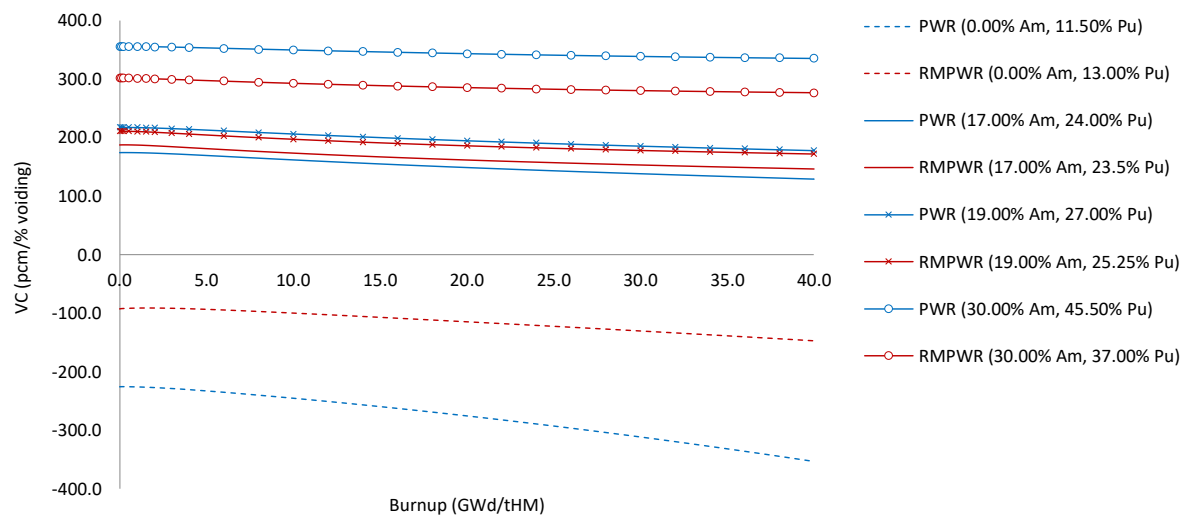
While these results show that changes in spectrum are important, they suggest that it would be possible to predict the effect of changing the fuel composition for a specific lattice type if a single case has been preliminarily analysed.

### 3.3. VC

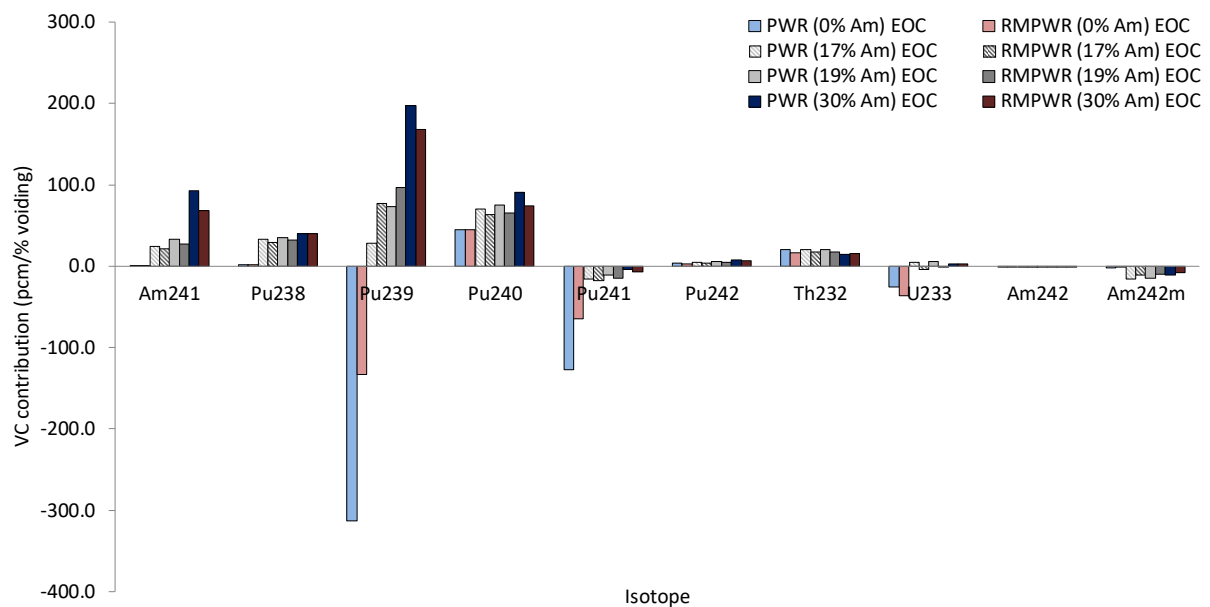
VC shows different trends to MTC. For lower Am content cases, VC is more negative in the PWR whereas, for higher Am content cases, VC is more negative/less positive in the RMPWR (Figure 9); the changeover occurs for an Am content of ~18%wt. For low Am content cases, the VC is negative because of large negative contributions from fissile isotopes; in contrast to the MTC case, this includes U233 (Figure 10). The negative contributions from Pu239 and Pu241 are significantly more negative in the PWR than the RMPWR, resulting in an overall more negative VC in the PWR. In higher Am content cases, almost all isotopes display a positive contribution. Am242m again provides a predictably negative contribution, although, due to the small quantities bred, the contribution has a negligible effect. The changeover, which occurs between 17 and 19%wt Am loading, is again caused by the difference in contributions from Pu239. In both the 17 and 19%wt Am cases, all fissionable isotopes display larger positive contributions to VC in the PWR while some fissile isotopes, i.e. Pu241 and U233, display less negative/more positive contributions in the PWR. In the 17% Am case, these effects are not sufficient to overcome the significant difference in contributions from Pu239, which is

notably less positive in the PWR than the RMPWR. However, in the 19% Am case, the difference in contributions from Pu239 in the PWR and RMPWR is less significant, resulting in the combined positive contributions from fissionable isotopes outweighing the effects of Pu239.

**Figure 9 Variation of VC (fully voided) with burnup for 0-30 %wt Am in the PWR and RMPWR**



**Figure 10 Major contributors to VC (fully voided) for selected cases**

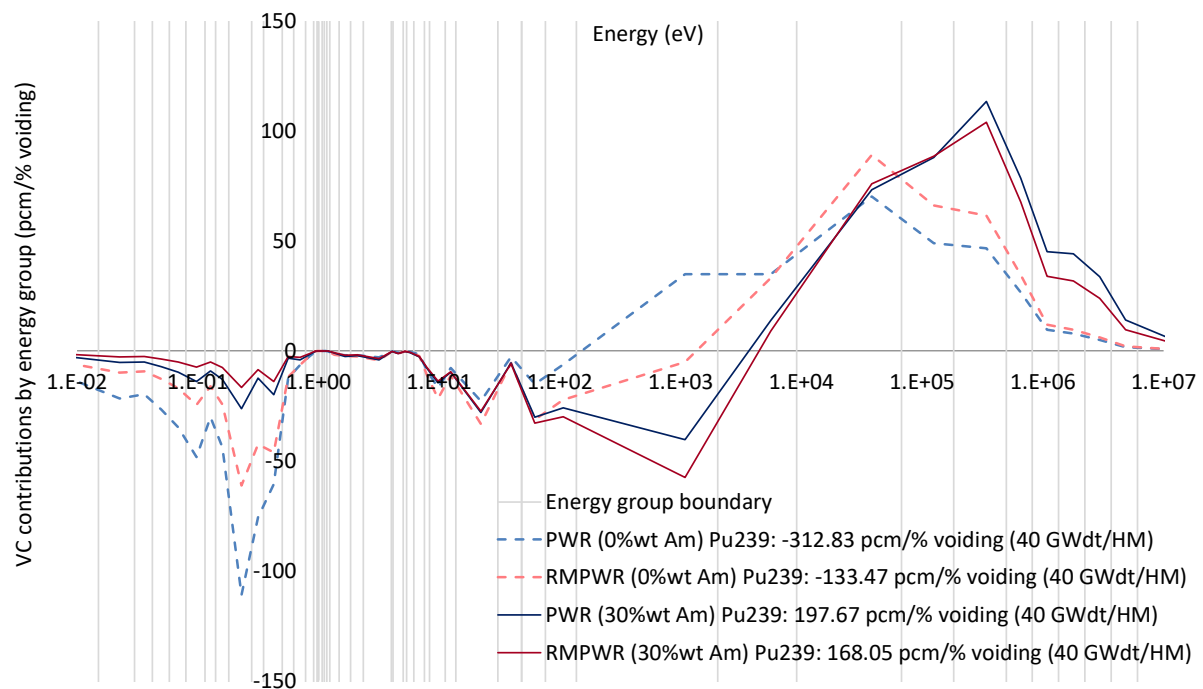


While the positive epithermal contributions from major isotopes are of a predictably large magnitude in all cases, due to the significant increase in the hardness of the spectrum as a result of the perturbation, the still relatively soft spectrum of the lower Am content cases means that the negative thermal contributions are dominant (Figure 11). In the PWR the negative thermal effects are particularly important due to the initially softer spectrum and the previously mentioned greater overall difference in microscopic cross section in the nominal and perturbed cases. As Am/Pu content increases, the negative effects are lost and the epithermal contributions and fast fission effects

dominate. The higher fissile fraction of the PWR fuel results in larger positive contributions in the higher energy region, causing the overall VC to be more positive in the PWR than the RMPWR. The reduction in thermal negative effects shows that, in order to maintain a negative VC, the total Am/Pu loading must remain relatively low or engineering safeguards must be put in place to mitigate against such a substantial loss of coolant. It may be possible to design a variable fuel enrichment loading pattern, through the use of spatial separation, which capitalises on the large negative contributions in the thermal region for low Am content cases and the more negative epithermal contributions in the RMPWR in high Am loading cases.

While the MTC and, to an extent, VC may appear more favourable in the PWR and higher fissile loadings appear acceptable in this lattice type, if the MTC and VC are limiting factors, it would be worth considering the total mass of Am/Pu loaded in each design. Since the diameter of the pins in the RMPWR is greater, it may be preferable to opt for low fissile loadings in the RMPWR to incinerate higher total masses. In addition, the incineration capability of the lattices should be considered, particularly with a view to not prohibiting multiple recycle schemes.

**Figure 11 Contributions to VC from Pu239 for 0 and 30%wt Am cases in the PWR and RMPWR at 40 GWd/tHM**



### 3.4. Incineration capabilities and effects of spatial separation

If the fresh fuel Pu vector was limited by the need to keep MTC and/or VC negative, the results suggest that the RMPWR would likely be the preferred option in both cases (Table 4). While the MTC and 90% VC were assumed to be 'hard limits' and were required to be negative throughout the cycle, the fully voided VC (99% VF) (i.e. an extreme LOCA) was deemed to be acceptable as long as it was not substantially positive at BOC and was negative by MOC. In the VC limited case, the Pu and Am incineration rates are comparable; however, the total mass of Pu loaded is higher in the RMPWR. The masses compared are for 1/3 core loading, as this is representative of how much fresh material would



be loaded when each new batch is added to the core (assuming a three-batch fuel management scheme). In the MTC limited case, the total mass of Pu loaded is comparable while the fraction of initial Am and Pu incinerated is higher in the RMPWR, particularly in the Am case. Options for spatial separation have therefore been considered using the RMPWR lattice with a TCUP fuel layout, and these have been compared to the original, uniformly loaded RMPWR case. In the TCUP design, the fissile loading, incineration capabilities and reactivity feedback coefficients have been considered for the three bounding cases for UK Pu (0 (clean), 3.91% (as is) and 5.60% (aged) Am) in either central or peripheral pins combined with two different 'high Am content' options (10 and 15% Am) in remaining pins (Table 5). The TCUP design has been limited to a maximum of 15%wt Am – which corresponds to ~20%wt total Pu – due to the previously mentioned need to keep the total fissile loading relatively 'low' in order to maximise the thermal negative reactivity effects in the large VC perturbation. This limit is also within theoretical fuel handling and manufacturing limits of 30%.

**Table 4 Pu and Am total mass loading and incineration capability for MTC and VC limiting cases**

Parameter	PWR		RMPWR	
	VC limited	MTC limited	VC limited	MTC limited
Total Am (%wt)	10.00	23.00	5.60	16.00
Total Pu (%wt)	17.00	33.50	15.75	22.50
Pu loaded (kg per 1/3 core)	4259.51	7367.76	5826.02	7429.19
Pu loaded (kg/assembly)	66.21	114.52	90.56	115.48
Pu burned (%)	21.84	8.96	23.14	14.50
Am loaded (kg per 1/3 core)	476.90	2217.58	345.61	1425.95
Am loaded (kg/assembly)	7.41	34.47	5.37	22.17
Am burned (%)	45.46	28.77	44.07	37.87
<i>VC (90% VF) (0 GWd/tHM)</i>	<i>-35.29</i>	<i>202.94</i>	<i>-8.56</i>	<i>122.08</i>
<i>VC (90% VF) (40 GWd/tHM)</i>	<i>-77.26</i>	<i>176.06</i>	<i>-49.24</i>	<i>85.23</i>
<i>VC (99% VF) (0 GWd/tHM)</i>	<i>13.06</i>	<i>284.10</i>	<i>26.28</i>	<i>173.68</i>
<i>VC (99% VF) (40 GWd/tHM)</i>	<i>-56.81</i>	<i>254.25</i>	<i>-31.55</i>	<i>131.03</i>
<i>MTC (0 GWd/tHM)</i>	<i>-37.32</i>	<i>-2.31</i>	<i>-28.27</i>	<i>-3.68</i>
<i>MTC (40 GWd/tHM)</i>	<i>-34.32</i>	<i>-1.93</i>	<i>-21.94</i>	<i>-2.33</i>

**Table 5 Pu and Am total mass loading and incineration capability for TCUP cases**

Parameter	0%C 10%P	3.91%C 10%P	5.60%C 10%P	0%C 15%P	3.91%C 15%P	10%C 0%P	10%C 3.91%P	10%C 5.60%P	15%C 0%P	15%C 3.91%P
Central location: Total Am (%wt)	0.00	3.91	5.60	0.00	3.91	10.00	10.00	10.00	15.00	15.00
Central location: Total Pu (%wt)	13.00	14.75	15.75	13.00	14.75	17.75	17.75	17.75	21.50	21.50
Peripheral location: Total Am (%wt)	10.00	10.00	10.00	15.00	15.00	0.00	3.91	5.60	0.00	3.91
Peripheral location: Total Pu (%wt)	17.75	17.75	17.75	21.50	21.50	13.00	14.75	15.75	13.00	14.75
Pu loaded (kg per 1/3 core)	5687.70	5909.84	6041.76	6185.90	6408.05	5617.36	5868.16	6017.11	6058.62	6309.43
Pu loaded (kg/assembly)	88.41	91.86	93.91	96.15	99.61	87.32	91.21	93.53	94.18	98.07
Pu burned (%)	23.82	22.25	21.36	20.74	19.41	24.24	22.47	21.48	21.32	19.82
Am loaded (kg per 1/3 core)	370.06	476.04	532.39	676.35	782.33	327.76	447.42	511.04	599.05	718.71
Am loaded (kg/assembly)	5.75	7.40	8.28	10.51	12.16	5.09	6.95	7.94	9.31	11.17
Am burned (%)	37.58	41.43	42.99	36.44	38.72	39.39	42.76	44.13	38.71	40.68
<i>VC (90% VF) (0 GWd/tHM)</i>	<i>-26.29</i>	<i>1.35</i>	<i>16.46</i>	<i>15.50</i>	<i>41.17</i>	<i>-29.48</i>	<i>-0.28</i>	<i>15.51</i>	<i>10.71</i>	<i>37.97</i>
<i>VC (90% VF) (40 GWd/tHM)</i>	<i>-59.90</i>	<i>-36.16</i>	<i>-23.65</i>	<i>-13.20</i>	<i>7.45</i>	<i>-65.76</i>	<i>-39.25</i>	<i>-25.49</i>	<i>-21.74</i>	<i>1.56</i>
<i>VC (99% VF) (0 GWd/tHM)</i>	<i>3.18</i>	<i>35.38</i>	<i>54.68</i>	<i>55.42</i>	<i>83.86</i>	<i>-2.02</i>	<i>32.72</i>	<i>53.26</i>	<i>48.19</i>	<i>79.07</i>
<i>VC (99% VF) (40 GWd/tHM)</i>	<i>-43.74</i>	<i>-14.33</i>	<i>1.18</i>	<i>16.48</i>	<i>40.73</i>	<i>-52.29</i>	<i>-18.87</i>	<i>-1.49</i>	<i>4.59</i>	<i>32.59</i>
<i>MTC (0 GWd/tHM)</i>	<i>-27.51</i>	<i>-24.36</i>	<i>-23.60</i>	<i>-22.16</i>	<i>-18.60</i>	<i>-28.09</i>	<i>-24.60</i>	<i>-23.85</i>	<i>-23.12</i>	<i>-19.14</i>
<i>MTC (40 GWd/tHM)</i>	<i>-23.09</i>	<i>-20.23</i>	<i>-18.66</i>	<i>-17.62</i>	<i>-14.70</i>	<i>-23.85</i>	<i>-20.64</i>	<i>-18.92</i>	<i>-18.74</i>	<i>-15.53</i>

The results show that there is no single 'best' solution; however, some options may be more attractive than others, depending on the main objective of the recycle. If the main purpose is to reduce the total Pu stockpile as quickly as possible, it may be desirable to consider the RMPWR uniformly loaded with 16%wt Am (MTC limited case) as this allows for the highest mass loading of Pu and Am for the cases considered. However, the VC is substantially positive for both 90 and 99% voiding. While measures can be taken to improve the VC through the use of burnable poisons (BPs) and engineering safeguards, these mitigations may introduce issues of their own which may need to be managed. For example, the use of BPs may result in increased Pu requirements to counteract suppression of keff and, since the total Pu %wt is already relatively high, this may lead to fuel fabrication issues. In addition, the use of engineering safeguards may result in additional manufacturing costs, licensing and/or technical challenges associated with relying on mechanical safety systems. It may therefore be worth considering reducing the fissile content in the fuel to improve VC.

In the TCUP assembly loaded with 3.91%wt (C) and 15%wt (P) Am, the mass of Pu and Am is higher than in the uniformly loaded RMPWR 5.60% Am (VC limited) case and the VC is significantly improved compared to the RMPWR 16%wt Am (MTC limited) case. Similarly, the %wt Pu and Am destroyed is greater than in the uniformly loaded MTC limited case, though it is reduced compared to the VC limited case. Placing the higher Am content pins in the centre of the TCUP assembly improves the VC compared to placing them in peripheral locations. While the VC is still positive, it is more favourable than in the MTC limited case, and would therefore require less significant reactivity controls.

If further improvements to VC are required, then other TCUP options may be considered. TCUP assemblies containing 0/15, 5.60/10 and 3.91/10 %wt Am all involve higher masses of Pu and Am than the VC limited RMPWR. The 5.60/10 %wt Am cases load comparable amounts of Pu to the 0/15 %wt Am cases, but the former have higher incineration rates. Where the higher Am pins are centrally located, the VC is negative for a burnup of 40 GWd/tHM for both 90 and 99% voiding cases, and this may lead to an overall negative core VC through the use of targeted batch management schemes.

If a negative VC is required for the entirety of the cycle in the 90% voiding case, then results suggest that the RMPWR 5.60% Am (VC limited) case would be preferable to the TCUP layout. The 0/10%wt Am TCUP design is the only TCUP option considered which achieves a consistently negative VC; however, the fissile mass and %wt Am destroyed are reduced compared to the RMPWR VC limited case.

Overall, the TCUP design shows some merit if the objective of a recycle scheme is to reduce the stockpile quickly. However, if the purpose is to maximise incineration potential, then the RMPWR VC limited case may be the preferred option. The %wt Pu burned is marginally higher in the 0/10% Am TCUP options, but the %wt Am destroyed is higher in the uniformly loaded RMPWR. This, coupled with a more complex fabrication process for the TCUP layout, may lead operators to choose the simpler design.

In terms of performing multiple recycles with each of these designs, the EOC Pu vector is not so dissimilar for each of the cases after a single stage recycle that any of the options considered would prohibit a second pass through the core. However, for the cases with higher Am content in the initial Pu vector, the total required Pu loading may become prohibitive after a certain number of passes. If

multiple recycles were to be pursued, the TCUP option would likely outperform the uniformly loaded RMPWR lattice due to its ability to target Am burning in higher Am, faster spectrum, central fuel pin locations, while using lower Am concentrations in softer spectrum, peripheral pins to maintain the desired large thermal negative contributions to VC.

#### **4. Conclusions**

Our previous research has shown how sensitive the limiting reactivity feedback coefficients, MTC and VC, are to isotopic and spectral effects in Th-Pu fuelled PWRs. This is because of the Pu239 content of the fresh fuel, which differs significantly between standard Pu grades and the predicted UK Pu vector. Where the Pu component of the fresh fuel remains relatively consistent – as in this study, where all Pu concentrations were based on UK Pu – and the isotopic variations are limited to changes in Am content in the fresh fuel, the response of the fuels to perturbations begins to display more predictable trends. The trends observed in this study may be used to predict how a given fuel type might respond if the Am/Pu content is altered – as long as an initial lattice physics study has been carried out. The results also show that, where a negative VC is required, operators may wish to limit the total fissile loading or attempt to make use of spatial separation, such that low Am/Pu loadings, with their larger thermal negative contributions to VC, are used to offset the dominant epithermal contributions to VC in higher Am/Pu content cases.

For the purposes of stockpile management, spatial separation of Am may offer some benefits over uniform loading of Am/Pu, depending on the purpose of the recycle scheme. Where the objective is to reduce the stockpile as quickly as possible and/or where multiple recycles are desirable, the TCUP layout with centrally located higher Am concentrations appears to be preferable in terms of maximising fissile mass loading – provided that a slightly positive VC at BOC can be tolerated or acceptably mitigated against, either through suitable batch management schemes or the addition of BPs and/or engineering safeguards. It should be noted that the cases considered in this study are by no means exhaustive and simply serve to illustrate potential options. Having identified the TCUP options which may be the most advantageous, decision-makers may wish to undertake a core loading pattern optimisation study to determine the ideal Am/Pu %wt and layout. Further spatial separation may be considered such that there are more than two types of fuel pin within the TCUP assembly, i.e. use of low, medium and high Am content pins. Part II of this study, which focusses on spatial separation of Am in BWRs, may provide preferable alternative options for Am recycle, if the UK decides to pursue this technology as opposed to or in addition to PWRs.

#### **5. Data availability statement**

To the best of the authors' knowledge, this paper and references herein contain all the data needed to reproduce and validate the results presented.

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